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Dynamic Aroma Release from Complex Food Emulsions

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Dynamic Aroma Release from Complex Food Emulsions

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1 Abstract

2 In-vitro dynamic aroma release over oil-in-water (o/w) and water-in-oil-in-water (w/o/w) 3 emulsions stabilised with Tween 20 or octenyl succinic anhydride (OSA) starch as a hydrophilic 4 emulsifier and polyglycerol polyricinoleate (PGPR) as a hydrophobic emulsifier was 5 investigated. The equal-molecular-weight hydrophilic aroma diacetyl (2,3-butanedione) or 6 relatively-more-hydrophobic 3-pentanone was added to the emulsions prepared by high 7 speed mixing, or membrane emulsification followed by thickened with xanthan gum 8 removing droplet size distribution and creaming as variables affecting dynamic release. 9 Results showed the differences of w/o/w emulsions in the dynamic release compared to o/w 10 emulsions mainly depended on aroma hydrophobicity, emulsion type, emulsifier-aroma 11 interactions and creaming. Xanthan led to a reduced headspace replenishment. Interfacially 12 adsorbed OSA starch and xanthan-OSA starch interaction influenced diacetyl release over 13 emulsions. OSA starch alone interacted with 3-pentanone. This study demonstrates the 14 potential impact of emulsifying and thickening systems on aroma release systems and highlights that specific interactions may compromise product quality. 15

16

17 Keywords: dynamic aroma release; OSA starch; xanthan gum; w/o/w emulsions

19 Introduction

20 The aroma of a processed food is one of the key quality parameters for its success in the 21 market place, and aroma release over simple oil-in-water (o/w) emulsions (for example, milk, cream, mayonnaise, salad dressing)¹ has been studied widely.²⁻⁹ Complex water-in-oil-in-22 23 water (w/o/w) emulsions are emulsions where the oil phase of o/w emulsions is partly 24 replaced by an inner aqueous phase. Due to the complex structure, w/o/w systems can be used for bioactive encapsulation.^{10, 11} w/o/w emulsions have been shown to have advantages 25 over o/w emulsions for fat reduction^{12, 13} and salt reduction.^{14, 15} Although food applications 26 in low calorie cream or fat-reduced mayonnaise,¹⁶ fat substitutes in meat emulsions,¹⁷ 27 substitutes for dairy fat in cheese¹² and so on have been reported, compared to o/w 28 29 emulsions aroma release over w/o/w emulsions has obtained far less attention in the published literature.^{18, 19} This might be at least in part due to the fact that w/o/w emulsions 30 31 are more difficult to stabilise than o/w emulsions. For the successful application in low-fat 32 and salt-reduced foods, an understanding of their aroma release properties is desirable.

33 The consumption of a food is a dynamic process as air is continuously exhaled and inhaled, rendering the acquisition of dynamic aroma release profiles more relevant to real foods, 34 compared to static methods. If the dynamic aroma release is only affected by oil, the ability 35 36 of an aroma compound to replenish a diluting headspace can be predicted by the equilibrium 37 headspace partition coefficient (water: air-water partition coefficient K_{aw}; emulsions: airemulsion partition coefficient K_{ae}).^{20, 21} A low K_{aw} or K_{ae} value will lead to a more stable 38 headspace concentration against headspace dilution.^{20, 21} In that case, K_{ae} is calculated by 39 Eq.1:²² 40

Eq.1

41
$$K_{ae} = \frac{1}{\frac{\Phi_o}{(K_{ao}} + \frac{\Phi_w}{K_{aw}})}$$

42 where Φ_{o} and Φ_{w} are the oil and water volume fraction respectively, K_{ao} is the air-oil 43 partition coefficient.

44 If there are other non-volatile solute-aroma interactions that limit aroma release to the headspace, the hypothesis is that there would be differences in the headspace replenishment 45 compared to the prediction by K_{ae} above. Factors such as emulsion composition and aroma 46 hydrophobicity (the octanol-water partition coefficient, log P or log K_{ow}) influence dynamic 47 48 aroma release over o/w emulsions.^{3, 4, 6-9} With regard to the impact of emulsion droplet size, 49 dispersed volume fraction and emulsifier concentration on dynamic aroma release, published 50 literature paints a controversial picture. On one hand side these factors are reported to have no impact,^{4, 6} on the other hand side impact of droplet size, affecting emulsion viscosity, on 51 dynamic aroma release has been reported.³ Further, decreasing release rates with increasing 52 53 fat level,⁹ decreasing lipophilicity⁹ and increasing gel strength⁸ for lipophilic compounds have 54 been reported. Undoubtedly, emulsifiers may interact with aroma compounds. For example, 55 micelles of low molecular weight (LMW) surfactants forming above their critical micelle concentration in solution can solubilise hydrophobic^{23, 24} or hydrophilic²⁵ molecules, or aroma 56 57 compounds as of interest in this study, in their core. Polymeric emulsifiers such as starches are known to interact with aroma compounds^{26, 27}. The suggested mechanisms is via hydrogen 58 bonding between the hydrophilic aroma compounds and the hydroxyl groups of starch,²⁸ or 59 60 inclusion complexes between the hydrophobic aroma compounds and amylose.²⁹ A 61 consequence of these interactions is that, when used as emulsifier, the relative distribution of interfacially adsorbed to non-adsorbed starch can affect aroma distribution in emulsions 62 and the headspace.^{24, 30-32} This ratio is affected by the total surface area of the dispersed 63

emulsion phase, thus the droplet size characteristics for emulsions formulated at the same dispersed phase volume. Nonetheless, there is a lack of understanding of how those factors impact on dynamic release over w/o/w emulsions and their release behaviour compared to o/w emulsions.

68 In this study, in-vitro dynamic headspace analysis was carried out to evaluate the 69 replenishment of two selected aroma compounds into the gas phase over w/o/w emulsions 70 compared to o/w emulsions during headspace dilution. Water controls were also analysed to 71 identify whether the emulsifier impacted dynamic aroma release. The overall aim of this study 72 was to investigate the dynamic aroma release behaviour in fat-reduced complex food 73 emulsions, w/o/w emulsions compared to o/w emulsions, and explore the emulsifier-aroma 74 interaction as well as emulsion microstructure (size distribution, droplet size, specific surface 75 area, Span and creaming) influence on dynamic release.

76

77 Materials and methods

78 Materials and sample composition

The oil phase in the emulsions comprised sunflower oil (density: 0.916±0.003 g/cm³; viscosity presented in supporting information Table S1) purchased from a local supermarket. All aqueous phases were prepared with deionised water unless otherwise stated. Polyoxyethylene 20 sorbitan monolaurate (Tween 20) (HLB = 16.7), diacetyl, 3-pentanone and sodium azide, added to prevent microbial spoilage, were obtained from Sigma Aldrich (Gillingham, UK), polyglycerol polyricinoleate PGPR (PGPR 90) from Danisco (Kettering, UK), octenyl succinic anhydride (OSA) starch (N-creamer 46) from Univar (Widnes, UK) and xanthan gum (Keltrol RD) from CP Kelco (San Diego, USA). Sodium chloride to aid
 microstructure stabilisation³³ was purchased from Fisher Scientific (Loughborough, UK). All
 concentrations are provided on a weight by weight basis, unless stated otherwise.

89 The composition of all liquid samples is listed in Table 1. Two hydrophilic emulsifiers including 90 the LMW surfactant Tween 20^{33, 34} and the polymeric emulsifier OSA starch^{14, 15} to stabilise 91 the external w/o/w emulsion interface were selected in this study to assess the interaction of 92 hydrophilic emulsifier type with aroma compounds and its impact on dynamic aroma release. 93 PGPR was chosen as the hydrophobic emulsifier due to most successfully stabilising w/o/w emulsions.³⁵ Simple o/w emulsions were included in the experimental design to compare with 94 95 w/o/w emulsions, formulated at the same dispersed phase volume of o and w/o respectively 96 in the emulsion system. Emulsions were initially processed with a high speed mixer. Then, 97 emulsions were also processed via a previously reported stirred cell membrane emulsification,³⁴ thereby removing droplet size variation as a factor impacting aroma release. 98 99 Since our initial analysis of the high speed processed emulsions suggested that droplet 100 creaming, which was observed for all emulsions produced, might have affected aroma release, 101 creaming was suppressed in the membrane processed emulsions by adding the viscosifying 102 agent xanthan gum. At the same time, PGPR was added also to the oil phase of the o/w 103 emulsions, although not required to stabilise an internalised aqueous phase, in order to retain 104 similarity in formulation for better comparison of the aroma release results. The thickened 105 emulsions had a comparatively lower dispersed phase volume due to the method of 106 preparation, outlined in the following.

107

108 Preparation of emulsions by high shear mixing

109 w/o/w emulsions

110	A two-step emulsification method with a batch high speed overhead mixer (L5M fitted with
111	emulsor screen, Silverson, Chesham, UK) was used to produce the w/o/w emulsions. Initially,
112	the internal w_1/o emulsion was prepared by slowly adding w_1 into oil while mixing at 7000
113	rpm for 4 min and cooling the process beaker (4-6 °C). Batch size was kept constant at 100 g
114	with a ratio of w_1 :0 of 2:3. This primary w/o emulsion was then added to w_2 during mixing at
115	6700 rpm for 4 min while cooling (4-6 °C). Batch size was also 100 g with a ratio of w_1 /o: w_2 of
116	3:7. Finally, 1 mL of aqueous sodium azide solution was added to the w/o/w emulsions to
117	obtain a final sodium azide concentration of 0.02% and the emulsion was stored at room
118	temperature (21 ± 5 °C) until further use.

119

120 o/w emulsions and water controls

o/w emulsions manufactured by high speed mixing were prepared by adding the oil to the
water. The same high speed overhead mixer as for preparation of the w/o/w emulsions was
used, operated at 6700 rpm for 4 min while cooling (4-6 °C). The mixing ratio of oil to water
was 3:7 and batches of 100 g were processed. The water controls contained Tween 20 or OSA
starch as the hydrophilic emulsifier at the same concentration as the external water phase of
w/o/w emulsions.

127

128 Preparation of xanthan gum thickened emulsions with stirred cell membrane emulsification

129 w/o/w emulsions

130 w/o/w emulsions were manufactured in two steps followed by the addition of xanthan gum. 131 First, w/o emulsions were produced by slowly adding w_1 into o under high shear mixing (Ultra 132 Turrax, model T25, IKA Works, Staufen, Germany) at 24000 rpm for 5 min while cooling the 133 process beaker (4-6°C). Batch size was kept constant at 100 g with a ratio of w_1 :o of 2:3. The 134 w/o/w emulsions were then manufactured using stirred cell membrane emulsification. w/o 135 emulsions were injected through a microporous membrane surface into the external aqueous 136 phase stirred by a paddle stirrer. Maximum shear stress at the membrane surface was 137 controlled by the rotational speed. The experimental conditions were a maximum shear stress 138 of 14 and 36 Pa for the continuous aqueous phase containing Tween 20 and OSA starch 139 respectively, and a constant w/o emulsion injection speed of 1 mL min⁻¹ corresponding to a transmembrane flux of 70 L h⁻¹ m⁻². The experiments were run until the dispersed phase 140 141 volume fraction reached 30 vol.% as determined by reading from the syringe scale. Batches 142 of 100 g were prepared, transferred into a glass beaker followed by the addition of 1 mL of 143 aqueous sodium azide solution to obtain a final sodium azide concentration of 0.02% and 144 stored at room temperature $(21 \pm 5 \degree C)$ until further use.

145

146 o/w emulsions

o/w emulsions manufactured by stirred cell membrane emulsification were prepared following the actual membrane emulsification step of preparing the w/o/w emulsions, with the difference that the dispersed phase corresponded to a single oil phase. In order to obtain a droplet size similar to that of the w/o/w emulsions, the process parameters were tested in preliminary experiments. These were a maximum shear stress at the membrane surface of 10 Pa and 36 Pa respectively for Tween 20 and OSA starch as emulsifier, and an oil phase injection
speed of 1 mL min⁻¹.

154

155 Xanthan gum solution preparation and addition

156 A 1% xanthan gum solution was prepared and added to the membrane processed w/o/w and 157 o/w emulsions as follows. Initially, the appropriate amount of xanthan gum was dispersed 158 into 0.1 M NaCl and 0.02% sodium azide solution pre-heated to 80 °C while stirring at 1500 159 rpm with an overhead mixer (RW20 fitted with a Propeller 4-bladed stirrer, IKA, Staufen, 160 Germany). Temperature was maintained at 80°C during 1 h of mixing after which the solution 161 was allowed to cool down at room temperature and left overnight for complete hydration 162 before use. 70 g of xanthan gum solution was then added to 100 g of membrane processed 163 emulsion sample contained in a 600 mL glass beaker followed by mixing at 600 rpm on a 164 magnetic stirrer for 30 min. The resulting xanthan gum concentration in the external aqueous phase of the w/o/w and o/w emulsions was 0.5%. 165

166 To prepare the xanthan gum thickened water controls, 100 g of the xanthan gum solution was

mixed with 100 g of w_2 at 600 rpm to also obtain a final xanthan gum concentration of 0.5%.

168

169 Emulsion characterisation

170 Emulsions were analysed immediately after manufacturing and then regularly during 6-day

171 storage at room temperature (21 ± 5 °C).

173 Microscopy

The microstructure of the w/o/w and o/w emulsions was visualised using bright field microscopy (EVOS FL, Life Technologies, USA). Slides were prepared by placing a small drop of emulsion diluted with water onto a glass slide and placed onto the optical stage without adding cover slips. Objective lenses x4, x10 and x20 were fitted and at least three randomly selected areas of each slide were imaged with each objective. Three slides were prepared for each emulsion.

180

181 Droplet size measurement

182 Droplet size distributions were acquired with a laser diffraction particle size analyser (Beckman-Coulter LS 13 320, Meritics Ltd, Dunstable, UK) fitted with a dispersion cell 183 containing deionized water. Measurement set up and analysis was controlled by the 184 185 instrument's software package. Once the emulsion was dispersed in the water, three 186 measurements were taken and the raw data was averaged before analysis based on the input 187 of the refractive indices of the dispersion medium (water; 1.33) and the dispersed phase (oil; 1.47). The absorption value of the dispersed phase was set to 0. Samples were prepared in 188 189 triplicates. The results are reported as the averaged droplet size distributions on a volume 190 basis, the mean droplet size on a volume basis $(d_{4,3})$, the specific surface area (SSA) and the 191 span of the monomodal size distributions.

192

193 *In-vitro* dynamic headspace analysis

194 A volume (95 mL) of w/o/w emulsion or o/w emulsion or water control were placed into a 195 134 mL total volume glass bottle with a 25 x 6 mm magnetic stirrer bar at the bottom and 196 stored at room temperature. Diacetyl or 3-pentanone was added to the liquid samples after, 197 rather than prior to, emulsion preparation, including addition of xanthan gum to the 198 membrane processed emulsions, in order to reduce aroma loss during processing due to 199 exposure to open air. These two aroma compounds were selected as they vary in log P (the 200 hydrophilic aroma, diacetyl: -1.34; the relatively more hydrophobic aroma, 3-pentanone: 0.75 201 estimated from EPI SUITE (EPA's and Syracuse Research Corp., USA) at 20 °C) whilst being 202 equal in molecular weight (diacetyl: 86.09 g/mol; 3-pentanone: 86.13 g/mol) to eliminate the 203 effect of molecular mass on aroma release. 400 µL L⁻¹ of aroma standard solution containing 204 0.1 M NaCI was prepared in a 100 mL volumetric flask. 5 mL of the aroma standard solution 205 was added into each bottle to obtain a final aroma concentration of 20 µL L⁻¹ in the liquid sample and a headspace volume of 34 mL. The bottles were immediately sealed and stirred 206 207 at 200 rpm for 1 min to ensure rapid distribution of the aroma compounds before the dynamic 208 headspace analysis. Samples were then allowed to equilibrate for at least 4 h at room 209 temperature (21 \pm 5 °C) to equilibrate aroma distribution between liquid and headspace. 4 h 210 was chosen because it was the minimum time required for the aromas to reach equilibrium, 211 as determined in preliminary tests. Samples were prepared in triplicate.

To dilute the headspace, nitrogen gas (N₂) was introduced into the bottle at a flow rate of 70 mL min⁻¹ measured using an electronic flow meter (vary-flow 500, Agilent Technologies, Berkshire, UK). 5 mL min⁻¹ of the gas phase was sampled into the APCI-MS (Ultima Micromass, Manchester, UK) over 10 min. The transfer line to the mass spectrometer was heated (140 °C) and the source was operated in positive ionisation mode (4kV corona discharge). The compounds were measured in selected ion mode at 87 mz⁻¹ (molecular weight +1) with a dwell time of 0.1 s. Raw data was exported to Excel (Microsoft Corporation) and graphs were
plotted as the average headspace intensity (%). The first peak of average headspace intensity
was set to 100%. The points measured after the first peak were divided by the first peak of
average headspace intensity.

222

223 Statistics

The mean values and their standard deviations were calculated using the spreadsheet software Microsoft Excel. Statistical analysis of the dynamic headspace intensity by MANOVA statistical analysis with least significant difference (LSD) post hoc test (p < 0.05) using the SPSS software (IBM Statistics 21, USA) at 2, 5 and 9 min, as early, mid and late stage of dynamic headspace analysis was carried out to explore significant differences in data sets.

229

230 Results and discussion

231 Emulsion characteristics

The o/w and w/o/w emulsions, stabilised with Tween 20 or OSA starch and processed by high speed or membrane emulsification, were viewed under a bright field microscope and it was confirmed that the expected emulsion structure had formed. The oil continuous droplet phase of the w/o/w emulsions showed their previously noted characteristic dark appearance (micrographs shown in supporting information Figure S1).³⁶ The volume based droplet size distributions of all of the prepared o/w and w/o/w emulsions are presented in Figure 1. The droplet size distribution of each type of the high speed mixed emulsions (Figure 1A) was

not affected by the choice of emulsifier. This indicates that the outcome of the high speed

240 process was controlled by the processing parameters rather than the emulsifier type and its 241 concentration. The droplet size distributions were broad showing a shoulder at smaller 242 droplet diameters, which was more pronounced for the o/w emulsions and shifted slightly to 243 larger droplet diameters for the w/o/w emulsions. With around 20 μ m, the main distribution 244 peak of the w/o/w emulsions was also slightly larger compared to 10 μ m for the o/w 245 emulsions. Since the same processing conditions were used for emulsifying the oil and the 246 w/o into their respective external emulsion phase, it can only be concluded that the increased 247 viscosity of the o/w emulsion compared to the oil (see supporting information Table 1), and 248 the additional presence of PGPR in the oil phase of the w/o/w emulsion led to this result. As 249 a consequence of these differences in droplet size distribution between the o/w and w/o/w 250 emulsions, the specific surface area of the oil droplets was larger in the case of the o/w 251 emulsions and thus the proportion of adsorbed emulsifier rendering the interpretation of 252 aroma release data in terms of aroma-emulsifier interactions challenging.

The droplet size distributions of the xanthan gum thickened membrane processed emulsions (Figure 1B) were monomodal and the volume based mean diameter, $d_{4,3}$, of all of these emulsions was approximately 60-70 µm resulting in the specific surface area of around 0.1 m² mL⁻¹, independent of the type of emulsion. Both types of Tween 20 stabilised emulsions had a span of around 0.6, whereas both types of OSA starch stabilised emulsions had slightly larger span of approximately 0.7.

All emulsions were tested in terms of microstructure stability by checking droplet size distribution over a storage period of 6 days, during which the aroma release experiments were conducted. There were no changes for any of the emulsions (data not shown for the sake of brevity). 263

264 Dynamic headspace analysis

The theoretical equilibrium headspace partition coefficients (K_{ae}) calculated by Eq.1 are reported in Table 2. According to Table 2, it is expected that if there were only oil-aroma interactions, diacetyl would most easily replenish the diluting headspace over water controls, then w/o/w and finally o/w emulsions. This would be the opposite for 3-pentanone. If the headspace replenishment did not meet that predicted by K_{ae}, this would suggest emulsifieraroma interactions and an impact of emulsion microstructure on dynamic release.

The first peak in the dynamic headspace analysis was effectively representative of the undiluted headspace and therefore regarded as the equilibrium headspace intensity, which was set to 100%. Afterwards the equilibrium was disturbed during headspace dilution, so the headspace intensity decreased over the course of the measurement. The values shown in the following were normalised by the first peak headspace intensity (signal = 100%).

276

277 High speed mixed emulsions

278 Diacetyl

Figures 2A and B show the changes of dynamic headspace intensity of diacetyl over water, the water controls and the emulsions for Tween 20 and OSA starch as emulsifier respectively. Across all samples, the diacetyl headspace intensity decreased by 20 to 40% during headspace dilution. Over water and water containing emulsifier (water controls), the diacetyl headspace intensity decreased initially but then stabilised at approximately 80%. According to the statistics reported in Table 3, the headspace concentration of all emulsions was significantly 285 lower than that over water at 9 min (p < 0.05). This behaviour was expected because 286 emulsions had higher air-emulsion partition coefficients than water as reported in Table 2.

Diacetyl initially showed less replenishment into the headspace over the o/w and w/o/w emulsions than water controls. Then the intensity of diacetyl progressively decreased more than over the water controls, without asymptotically reaching an equilibrium value. In Table 3, at 2 min and for Tween 20 as surfactant, the diacetyl concentration over the o/w emulsion was higher than that over the w/o/w emulsion (p < 0.05). Thus, the fat-reduced w/o/w emulsion system showed an inhibition of the dynamic diacetyl release compared to the o/w emulsion.

294 Aroma release under dynamic condition is mainly affected by the air-liquid interface, as this 295 interface replenishes the headspace with volatile compounds as the headspace is diluted. All 296 of the high speed mixed emulsions creamed; a cream phase on top and a serum phase at 297 bottom was observed visually. Hence, underneath the layer of emulsifier molecules at the air-298 emulsion interface there was a layer of creamed oil droplets representing an additional 299 barrier affecting aroma release. Due to the broad droplet size distribution (Figure 1), the 300 creamed layer of oil droplets would have contained larger droplets towards its top and 301 smaller droplet towards its bottom. So the higher diacetyl release over the o/w emulsion 302 contrary to expectation was probably due to the cream layer acting as a barrier for diacetyl 303 movement from the continuous water phase underneath the creamed oil droplets. The 304 thickness of the cream layer was different between the emulsions due to the difference in 305 the droplet size, size distribution and density in addition to the viscosity of the continuous phase. The w/o/w emulsions had a thicker cream layer due to their larger main distribution 306 307 peak compared to the o/w emulsions (Figure 1), leading to the poorer headspace

308 replenishment of diacetyl over the w/o/w emulsions. Another reason could be the presence 309 of PGPR in the oil phase of the w/o/w emulsions, which was absent in the o/w emulsions. 310 PGPR could have trapped diacetyl molecules, partitioned into the oil phase, in the hydrophilic 311 core of their micelles thereby slowing transfer into the aqueous phase as a result of 312 equilibrium disturbance and ultimately aroma release.

313 However, the release of diacetyl over the o/w emulsion and the w/o/w emulsion was not 314 different for the OSA starch as emulsifier (Table 3). Hence, the w/o/w emulsion had a similar 315 ability to maintain the headspace concentration of diacetyl as the o/w emulsion. This could 316 be because diacetyl interacted with the interfacially adsorbed starch at the oil-water 317 interface. There was a higher amount of the starch adsorbed at the creamed oil droplet 318 interface of o/w emulsions than that of the w/o/w emulsions due to its smaller main 319 distribution peak (Figure 1) resulting in a larger SSA of o/w emulsions, which led to no 320 significant difference in the diacetyl release over OSA starch stabilised o/w and w/o/w 321 emulsions.

In summary, the dynamic release behaviour of diacetyl over high speed mixed emulsions was
 mainly driven by emulsion type, creaming resulting from the broad droplet size distribution
 and SSA of the emulsion characteristics and diacetyl-OSA starch interactions.

325

326 3-pentanone

Figures 2C and D show the changes of dynamic headspace intensity of 3-pentanone over emulsions and water controls. The headspace intensity decreased by 20% to 60 % for 3pentanone during headspace dilution for all samples. This was more than for diacetyl (Figures 2A and B), the lower headspace replenishment would be caused by 3-pentanone's higher K_{aw}

331 compared to diacetyl (Table 2). The water control and the emulsifier alone showed an initial 332 major decrease in headspace intensity, which stabilised at about 40%. As expected in Table 333 2, they had the lowest headspace 3-pentanone intensity over time, which suggests the 334 weakest headspace replenishment among all samples. As reported in Table 4, OSA starch 335 alone led to a significant decrease in the dynamic headspace intensity compared to the water 336 control at 2, 5 and 9 min (p < 0.05), which suggests an interaction of starch with 3-pentanone 337 possibly through hydrophobic interaction or a starch barrier effect at the air-water interface 338 reducing volatile movement.

339 According to Figures 2C and D and Table 4, 3-pentanone had the strongest headspace 340 replenishment (p < 0.05) over the o/w emulsions over 10 min without asymptotically reaching 341 an equilibrium value, then w/o/w emulsions and last water. It met the expectation as K_{ae} 342 predicts in Table 2. It has been reported previously that an o/w emulsion system stabilised 343 the hydrophobic aroma headspace concentration during headspace dilution relative to the 344 water system^{37, 38} as a direct result of the emulsion decreasing the air-liquid partition 345 coefficient. There was no significant difference among o/w or w/o/w emulsions (Table 4). This 346 is probably due to 3-pentanone favouring oil so the oil phase played a major role in 3-347 pentanone release and the hydrophilic emulsifier type could not limit the headspace intensity. 348 The cream layer of the emulsions could facilitate the replenishment of 3-pentanone into the 349 gas phase during headspace dilution.

Thus, the dynamic release behaviour of 3-pentanone over high speed mixed emulsions wasmainly driven by emulsion type and creaming.

353 Membrane processed and xanthan gum thickened emulsions

354 Diacetyl

355 Figures 3A and B reveal the dynamic headspace release of diacetyl over xanthan gum-356 thickened samples. The headspace intensity decreased by approximately 40% for diacetyl 357 during dilution for all samples. All samples showed a progressive decrease in the headspace 358 intensity without asymptotically reaching an equilibrium value. The xanthan gum thickened 359 water had a lower headspace intensity at mid and late stage compared to water in the 360 absence of xanthan gum (Figures 2A and B). This was probably caused by the xanthan gum 361 increasing the viscosity of the water (supporting information Table S1) such that the xanthan 362 gum network at the air-water interface delayed the release of diacetyl. It has been reported 363 that significant binding of all tested compounds (diacetyl, 1-octen-3-ol, diallyl sulfide, diallyl disulfide) occurred at 0.1% xanthan under equilibrium headspace analysis and hydrogen 364 365 bonding was found in 1-octen-3-ol-xanthan interactions by exclusion chromatography.³⁹ It 366 can be speculated that hydrogen bonding between diacetyl and xanthan gum may also have 367 occurred.

For Tween 20 (Table 5), diacetyl showed the most stable headspace intensity over water and Tween 20 alone, then w/o/w and last o/w emulsions. This is as expected on the basis of the K_{ae} values. For the membrane emulsification processed and xanthan gum thickened emulsions, creaming was reduced due to the increased viscosity of the continuous aqueous phase (supporting information Table S1). The impact of emulsion microstructure on dynamic release was also minimised because all the emulsions had a similar size distribution (Figure 1), droplet size, SSA and a low Span. The emulsion droplets were homogenously dispersed in the continuous water phase. Hence, oil was the only factor influencing on the diacetyl releaseover water and emulsions in the presence of Tween 20.

377 For OSA starch (Table 5), the OSA starch and xanthan gum water control showed a 378 significantly lower headspace concentration than the xanthan gum alone only at 2 min (p < 1379 0.05), which indicates an interaction of diacetyl with OSA starch or with OSA starch and 380 xanthan gum. It was reported above that there was no interaction of diacetyl with OSA starch 381 under dynamic headspace conditions in the absence of xanthan gum. Therefore, this 382 interaction of diacetyl was associated with xanthan gum and OSA starch. Furthermore, the 383 viscosity of these water controls and emulsions was measured revealing an interaction of xanthan gum with OSA starch as its addition lowered the viscosity of the xanthan gum 384 385 (supporting information Table S1). Thus, a xanthan gum-OSA starch interaction influenced the 386 dynamic release of diacetyl. However, there was no significant difference among o/w or 387 w/o/w emulsions. Hence, interaction of diacetyl with xanthan gum and OSA starch appeared 388 to be absent in o/w and w/o/w emulsions (Table 5). It is worth noting thought that in the 389 presence of xanthan gum the viscosity of the OSA starch stabilised emulsions was lower 390 compared to those stabilised with Tween 20 (supporting information Table S1). Consequently, 391 while xanthan gum-OSA starch interactions are evident, these did not impact on the dynamic 392 release of diacetyl in the emulsion systems whereas they did in the control system. Further 393 detailed analysis of this system is required to understand why the fact that a proportion of 394 the OSA starch molecules adsorbed at the oil droplet interface, therefore not available to 395 interact with xanthan gum, might be the reason for the dynamic release of diacetyl 396 observation.

Hence, the dynamic release behaviour of diacetyl over membrane processed and xanthan
gum thickened emulsions was mainly driven by emulsion type and interactions between
diacetyl and xanthan-OSA starch association.

400

401 *3-pentanone*

402 Figures 3C and D show the changes of dynamic headspace of 3-pentanone over xanthan gum 403 thickened samples. The headspace intensity decreased by approximately 60% for 3-404 pentanone during dilution for all samples. All samples also showed a progressive decrease in 405 the headspace intensity without asymptotically reaching an equilibrium value. The xanthan 406 gum thickened emulsions had no difference in dynamic headspace intensity with the xanthan 407 gum solution (Table 6). They also showed a much weaker resistance to dilution compared 408 with the high speed mixed emulsions (Figure 2C and D). This may have been due to diffusion barriers that limited headspace replenishment,⁸ or increased viscosity⁴⁰ that decreased 409 410 droplet mobility, or, abundance of droplets at the air-emulsion interface. The droplets in high 411 speed mixed emulsions on the other hand were more mobile as these emulsions were not 412 thickened and 3-pentanone continually released into the headspace. There was no significant 413 factor influencing the dynamic release behaviour of 3-pentanone over membrane processed 414 and xanthan gum thickened emulsions.

415

416 Conclusions

The conclusions that could be drawn based on the experimental data acquired in this studyare summarised in Table 7. Xanthan gum led to a reduced aroma headspace replenishment

419	mainly due to the effect of increased viscosity. OSA starch alone interacted with 3-pentanone
420	possibly through hydrophobic interaction or a starch barrier effect. Dynamic diacetyl release
421	was affected by the OSA starch adsorbed at the oil-water interface and xanthan gum-OSA
422	starch interaction. This study demonstrates the potential impact of emulsifying and
423	thickening systems on aroma release systems and highlights that specific interactions may
424	compromise product quality.
425	
426	Acknowledgement and Declaration
427	Pu acknowledges a scholarship from China Scholarship Council (CSC).
428	
429	Supporting Information
430	Micrographs of high speed mixed or membrane processed and xanthan thickened w/o/w and
431	o/w emulsions, see Figure S1.
432	Viscosity results of oil and external water phase of w/o/w emulsions and xanthan gum
433	thickened w/o/w emulsions, see Table S1.
434	This material is available free of charge via the Internet at
435	https://nam02.safelinks.protection.outlook.com/?url=http%3A%2F%2Fpubs.acs.org&d
436	ata=02%7C01%7C%7C2dd9e187411645add5c408d709dcf7b2%7C84df9e7fe9f640afb435aaa
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438	6tglN7F256Vi0FTulnuAI%3D&reserved=0.

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547	List of figure	captions
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Figure 1 Averaged droplet size distributions on a volume basis of A) high speed mixed or B)
membrane processed and xanthan thickened o/w (ow) and w/o/w (wow) emulsions stabilised
with Tween 20 (T) or OSA starch (S): □ Day of making; ■ Day 6.

551

- 552 Figure 2 Dynamic headspace intensity of A, B) diacetyl or C, D) 3-pentanone above xanthan
- 553 gum thickened water (w), o/w (ow) emulsions and w/o/w (wow) emulsions stabilised with A,
- 554 C) Tween 20 (T) or B, D) OSA starch (S). Values are based on 3 replicates.

555

- 556 Figure 3 Dynamic headspace intensity of A, B) diacetyl or C, D) 3-pentanone above xanthan
- 557 gum thickened water (w), o/w (ow) emulsions and w/o/w (wow) emulsions stabilised with A,
- 558 C) Tween 20 (T) or B, D) OSA starch (S) in the absence or presence of xanthan gum (XG). Values
- 559 are based on 3 replicates.

Table 1 Composition of w/o/w and o/w emulsions and water control. w_1 : the internal water phase. w_2 : the external water phase. T20: Tween 20. S: OSA starch. XG: xanthan gum. For each emulsion, the dispersed phase mass fraction of the xanthan gum thickened membrane processed emulsions lowered compared to that of high shear mixed emulsions due to the experiment design.

sample ID	W ₁	composition	oil	composition	W ₂	composition of w_2
	(wt.%)	of w ₁	(wt.%)	of oil	(wt.%)	
wT	-	-	-	-	100	2% T20, 0.1 M NaCl
wS	-	-	-	-	100	4% S, 0.1 M NaCl
owT	-	-	30	-	70	2% T20
owS	-	-	30	-	70	4% S
wowT	12	0.1 M NaCl	18	4% PGPR	70	2% T20, 0.1 M NaCl
wowS	12	0.1 M NaCl	18	4% PGPR	70	4% S, 0.1 M NaCl
XG	-	-	-	-	100	0.5 % XG
wT+XG	-	-	-	-	100	2% T20, 0.1 M NaCl,
						0.5 % XG
wS+XG	-	-	-	-	100	4% S, 0.1 M NaCl, 0.5 %
						XG
owT+XG	-	-	18	4% PGPR	82	1% T20, 0.1 M NaCl
						0.5 % XG
owS+XG	-	-	18	4% PGPR	82	2% S, 0.1 M NaCl, 0.5 %
						XG
wowT+XG	7	0.1 M NaCl	11	4% PGPR	82	1% T20, 0.1 M NaCl
						0.5 % XG
wowS+XG	7	0.1 M NaCl	11	4% PGPR	82	2% S, 0.1 M NaCl, 0.5 %
						XG

Table 2 Theoretical equilibrium headspace partition coefficients (K_{ae}) of two aroma compounds, diacetyl and 3-pentanone, calculated by Eq.1 at 20 °C under dynamic headspace analysis conditions: water: air-water partition coefficient (K_{aw}) estimated from EPI SUITE (EPA's and Syracuse Research Corp., USA) at 20 °C.; emulsions: air-emulsion partition coefficient. XG: xanthan gum.

XG addition	aroma type	water	o/w emulsion	w/o/w emulsion
No XG	diacetyl	5.4x10 ⁻⁴	7.6x10 ⁻⁴	6.6x10 ⁻⁴
	3-pentanone	3.6x10 ⁻³	1.5x10 ⁻³	2x10 ⁻³
+XG	diacetyl	5.4x10 ⁻⁴	6.5x10 ⁻⁴	6.1x10 ⁻⁴
	3-pentanone	3.6x10 ⁻³	2x10 ⁻³	2.4x10 ⁻³

561

Table 3 Dynamic headspace intensity (%) of diacetyl above water (w), o/w (ow) and w/o/w (wow) emulsions stabilised with Tween 20 (T) or OSA starch (S) at 2, 5 and 9 min during headspace dilution. The headspace intensity at the first time point was set to 100%.

Samples	2 min	5 min	9 min
water	83.9±1.0 ^{a*}	80.4±1.9ª	80.4±1.9ª
wT	82.8±1.4 ^{ab}	80.6±3.1ª	81.0±3.9ª
wS	81.1±2.5 ^{ab}	76.8±1.2 ^{ab}	79.9±7.8ª
owT	85.0±3.4ª	77.9±3.5 ^{ab}	70.3±3.9 ^b
owS	84.7±1.9ª	75.0±3.7 ^{ab}	67.8±4.1 ^b
wowT	78.9±3.1 ^b	73.0±6.2 ^b	66.0±5.9 ^b
wowS	83.0±0.7ª	75.9±2.4 ^{ab}	68.5±1.7 ^b

Values for relative headspace intensity are the mean of 3 replicates ± the standard deviation.

* Within a column, different letters indicate statistically significant values (p < 0.05).

Table 4 Dynamic headspace intensity (%) of 3-pentanone above water (w), o/w (ow) and w/o/w (wow) emulsions stabilised with Tween 20 (T) or OSA starch (S) at 2, 5 and 9 min during headspace dilution. The headspace intensity at the first time point was set to 100%.

Samples	2 min	5 min	9 min
water	58.0±1.7 ^{a*}	48.6±1.7ª	45.0±1.7 ^b
wT	52.6±2.5 ^{ab}	44.7±3.5 ^{ab}	42.0±4.7 ^b
wS	50.9±1.4 ^b	40.2±0.2 ^b	35.3±0.4ª
owT	87.4±0.8 ^d	78.6±1.5 ^d	70.6±1.3 ^d
owS	89.4±7.9 ^d	77.1±7.4 ^d	67.3±6.5 ^d
wowT	73.1±0.2 ^c	62.1±2.7 ^c	53.0±3.7 ^c
wowS	72.1±2.2 ^c	59.7±2.6 ^c	51.1±2.4 ^{bc}

Values for relative headspace intensity are the mean of 3 replicates ± the standard deviation.

* Within a column, different letters indicate statistically significant values (p < 0.05).

Table 5 Dynamic headspace intensity (%) of diacetyl above xanthan thickened (+XG) water (w), o/w (ow) and w/o/w (wow) emulsions stabilised with Tween 20 (T) or OSA starch (S) at 2, 5 and 9 min during headspace dilution. The headspace intensity at the first time point was set to 100%.

-			
Samples	2 min	5 min	9 min
w+XG	89.0±1.0 ^{ab*}	79.5±1.2ª	70.2±2.5 ^{ab}
wT+XG	90.0±1.4ª	79.8±3.4ª	72.4±4.1 ^a
wS+XG	79.5±1.9 ^{cd}	73.8±3.8 ^{ab}	68.2±6.5 ^{ab}
owT+XG	80.1±4.2 ^{cd}	69.4±5.2 ^b	63.6±4.0 ^{ab}
owS+XG	75.7±2.2 ^d	68.4±3.3 ^b	63.2±4.3 ^b
wowT+XG	83.7±4.0 ^{bc}	74.4±4.7 ^{ab}	67.7±6.6 ^{ab}
wowS+XG	79.4±5.7 ^{cd}	73.5±4.0 ^{ab}	68.5±6.0 ^{ab}

Values for relative headspace intensity are the mean of 3 replicates ± the standard deviation.

* Within a column, different letters indicate statistically significant values (p < 0.05).

Table 6 Dynamic headspace intensity (%) of 3-pentanone above xanthan thickened (+XG) water (w), o/w (ow) and w/o/w (wow) emulsions stabilised with Tween 20 (T) or OSA starch (S) at 2, 5 and 9 min during headspace dilution. The headspace intensity at the first time point was set to 100%.

Samples	2 min	5 min	9 min
w+XG	64.1±2.0 ^{ab*}	49.7±2.0 ^{ab}	39.1±1.0 ^{ab}
wT+XG	60.6±4.9 ^{ab}	49.9±2.6 ^{ab}	38.8±1.3 ^{ab}
wS+XG	61.4±6.0 ^{ab}	47.7±2.9ª	34.9±2.1ª
owT+XG	67.1±4.1ª	51.6±4.8 ^{ab}	39.8±4.0 ^{ab}
owS+XG	56.6±6.0 ^b	44.8±6.3ª	35.8±4.7ª
wowT+XG	69.0±6.3ª	56.4±5.2 ^b	44.5±2.8 ^b
wowS+XG	60.0±6.9 ^{ab}	44.9±3.3ª	38.7±5.0 ^{ab}

Values for relative headspace intensity are the mean of 3 replicates ± the standard deviation.

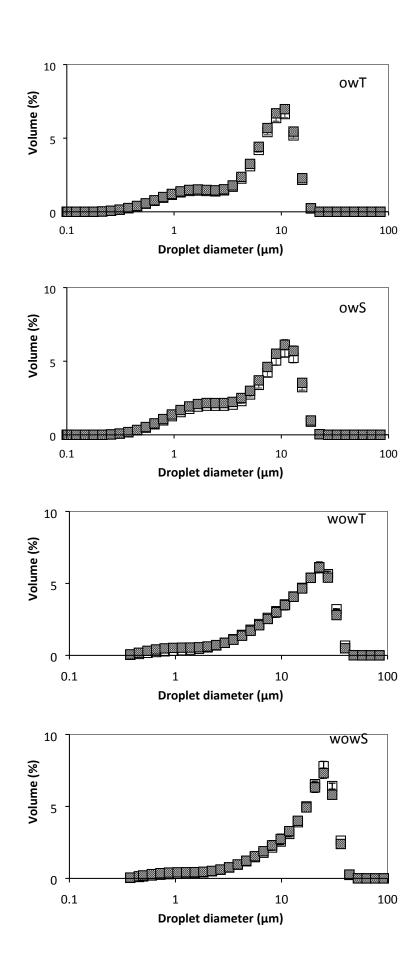
* Within a column, different letters indicate statistically significant values (p < 0.05).

Table 7 Results summary of the inhibition, enhancement or similar ability of w/o/w emulsions in the dynamic headspace release of diacetyl or 3-pentanone compared to o/w emulsions and the main factors driving the phenomenon. A) High speed mixed or B) membrane processed and xanthan gum thickened emulsions stabilised with Tween 20 or OSA starch as the hydrophilic emulsifier.

Preparation method	Aroma compounds	Tween 20	OSA starch	Main factors
A)	Diacetyl	Inhibition	Similar	Emulsion type, creaming and diacetyl-OSA starch interactions
	3-pentanone	Inhibition	Inhibition	Emulsion type and creaming
В)	Diacetyl	Enhancement	Similar	Emulsion type and diacetyl- xanthan gum-OSA starch interactions
	3-pentanone	Similar	Similar	None

Figure 1 Page 1

A)



33 ACS Paragon Plus Environment

B)

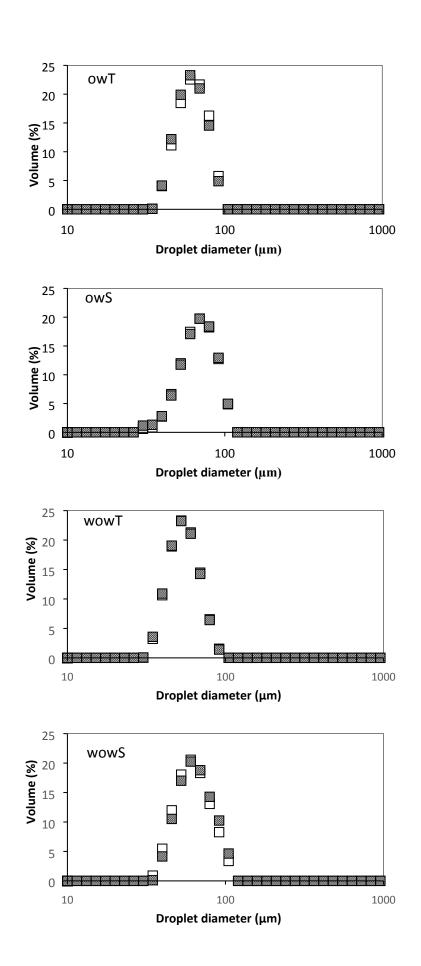
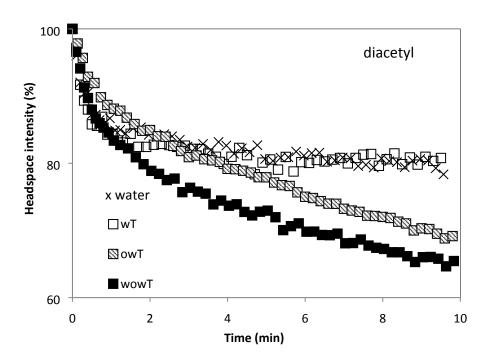




Figure 1 Page 3

Figure 1 Averaged droplet size distributions on a volume basis of A) high speed mixed or B) membrane processed and xanthan thickened o/w (ow) and w/o/w (wow) emulsions stabilised with Tween 20 (T) or OSA starch (S): \Box Day of making; \blacksquare Day 6.

A)



B)

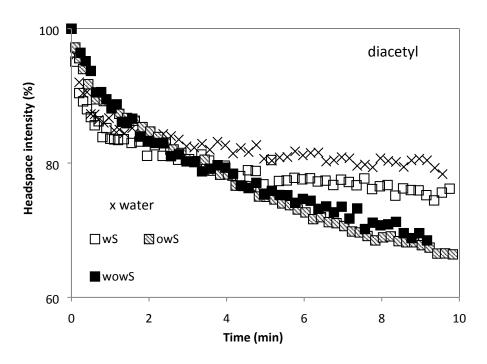
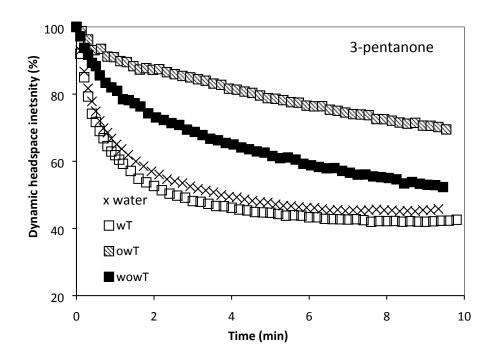


Figure 2 Page 2

C)



D)

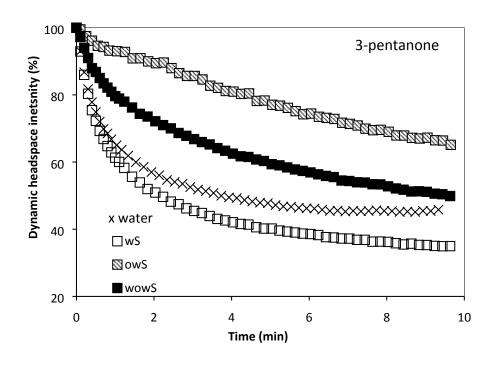
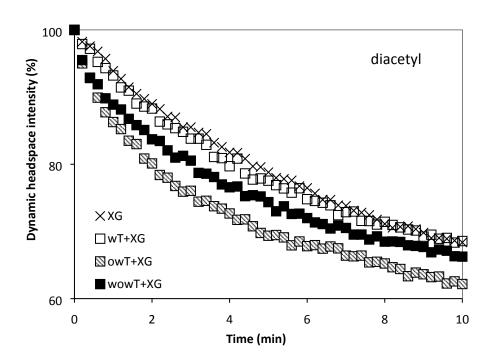


Figure 2 Dynamic headspace intensity of A, B) diacetyl or C, D)3-pentanone above xanthan gum thickened water (w), o/w (ow) emulsions and w/o/w (wow) emulsions stabilised with A,C) Tween 20 (T) or B, D) OSA starch (S). Values are based on 3 replicates.

A)



B)

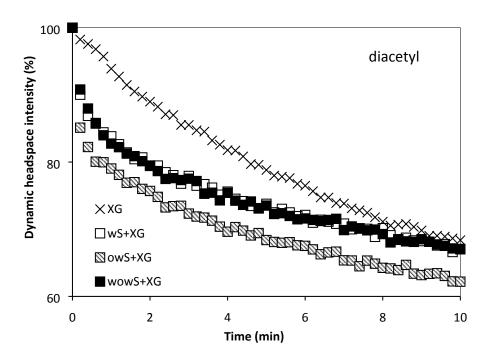
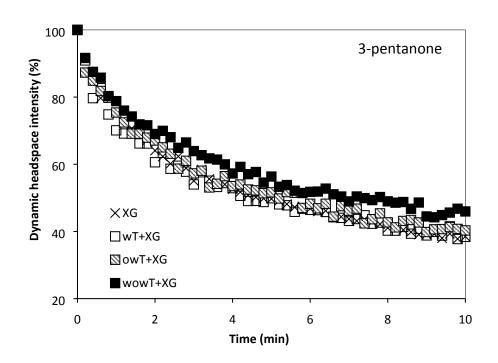


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C)



D)

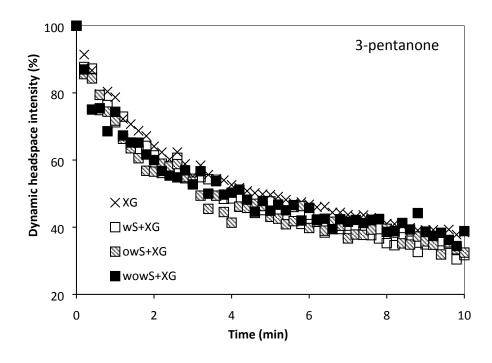


Figure 3 Dynamic headspace intensity of A, B) diacetyl or C, D) 3-pentanone above xanthan gum thickened water (w), o/w (ow) emulsions and w/o/w (wow) emulsions stabilised with A,

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C) Tween 20 (T) or B, D) OSA starch (S) in the absence or presence of xanthan gum (XG). Values

are based on 3 replicates.

TOC graphic

