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# **Magnetically Modified Electrocatalysts for Oxygen Evolution Reaction in Proton Exchange Membrane (PEM) Water Electrolyzers**

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## ABSTRACT

Green hydrogen production can only be realized via water electrolysis using renewable energy sources. Proton exchange membrane water electrolyzers have been demonstrated as the technology of choice for mass production of green hydrogen due to their scalability and potential high efficiency. However, the technology is still relatively expensive due to the catalyst materials cost and operational limitations due to mass transfer and activation polarizations. During the oxygen evolution reaction, oxygen bubbles stick to the electrode surface and this causes a low reaction rate and high mass transfer losses. In this study, the commonly used electrocatalyst for oxygen evolution reactions;  $\text{IrO}_2$ , is modified by introducing magnetic  $\text{Fe}_3\text{O}_4$  to achieve greater bubble separation at the anode during operation. The prepared composite catalysts were characterized using Scanning Electron Microscope, Energy Dispersive X-Ray Analysis, X-Ray Powder Diffraction, X-ray photoelectron spectroscopy and Brunauer–Emmett–Teller characterization methods. The modified composite electrocatalyst samples are magnetized to investigate the magnetic field effect on oxygen evolution reaction performance in proton exchange membrane water electrolyzers. 90%  $\text{IrO}_2$  - 10%  $\text{Fe}_3\text{O}_4$  and 80%  $\text{IrO}_2$  - 20%  $\text{Fe}_3\text{O}_4$  samples are tested via linear sweep voltammetry both ex-situ and in-situ in a proton exchange membrane water electrolyzer single cell. According to the linear sweep voltammetry tests, the magnetization of the 80%  $\text{IrO}_2$  - 20%  $\text{Fe}_3\text{O}_4$  sample resulted in 15% increase in the maximum current density. Moreover, the single cell electrolyzer test showed a four-fold increase in current density by employing the magnetized 80%  $\text{IrO}_2$  - 20%  $\text{Fe}_3\text{O}_4$  catalyst.

**Keywords:** Electrocatalysts, Kelvin Force, Lorentz Force, Magnetic Field, PEM Water Electrolyzer

## 1. Introduction

The global energy demand is dependent on fossil fuels causing environmental problems due to the emission of harmful greenhouse gases (GHG) such as  $\text{SO}_x$ ,  $\text{C}_n\text{H}_m$ ,  $\text{NO}_x$  and  $\text{CO}_x$ . Thus, meeting the global energy demand from clean and renewable energy sources has become an international target with many countries committed to achieving it [1]. Hydrogen is an energy carrier that has higher specific energy density than any fossil fuel and no associated GHG emissions, which makes it an ideal candidate for storing renewable energy and replacing fossil fuels [2]. Among the various hydrogen energy production technologies, Proton Exchange Membrane Water Electrolyzer (PEMWE) has promising advantages due to its high efficiency and possibility to integrate with renewable energy sources such as solar, wind, wave, etc. [3-6]. The main barrier for PEMWEs commercialization is their high cost due to the use of expensive metallic electrocatalysts for oxygen evolution reaction (OER) and hydrogen evolution reaction (HER) at the anode and cathode respectively [7-11]. At the cathode, Pt catalyst is commonly used while metal oxides, namely;  $\text{IrO}_2$  and  $\text{RuO}_2$ , are used at the anode providing high kinetic activity and durability [3, 12-15]. The literature indicates that  $\text{IrO}_2$  is more durable than  $\text{RuO}_2$  in an acidic environment however  $\text{RuO}_2$  is more active for the OER. Thus, composite catalysts combining different noble metals or noble metals with non-noble metals have been explored [3, 16].

During operation, PEMWE suffer performance losses due to activation, ohmic and concentration overpotentials. The low activity of the electrocatalyst at the electrodes results in activation overpotentials. Ohmic losses are due to contact and internal resistances within the cell components. Finally, concentration overpotentials are the result of limitations in species mass transport from and to the active sites at the electrode. In PEMWE, bubbles are formed from the OER and HER reactions covering the electrical double layers and causing

concentration losses. The ability of the electrode to remove the formed bubbles is affected by the electrode surface, materials and the electrode geometry [17, 18].

During the OER in a PEMWE, the formed oxygen bubbles stick to the electrode surface causing a loss of active surface area and high mass transport overpotential [19]. Therefore, research were conducted on modifying the cell design to facilitate oxygen bubbles removal from the electrode surface and maintaining high performance especially at high current densities. The effect of external environments such as; microgravity, centrifugal force, ultrasonic and magnetic fields were investigated for aqueous water electrolyzers in order to achieve and maintain bubble free electrodes during the electrolyzer operation [20-24]. For example, Kiuchi et al. [23] investigated the galvanostatic water electrolysis under microgravity. They concluded that bubbles are attached to the electrode surface more than standard gravity conditions causing higher ohmic resistance inside the cell. In another study Lao et al. [25] investigated the centrifugal force effect on alkaline water electrolysis. They obtained almost three-fold increase in current density in centrifuged electrolysis conditions. Li et al. [26] investigated the presence of ultrasonic field on the water electrolyzers performance. They concluded that ultrasonic water electrolysis increases hydrogen production efficiency by 5-18%.

Among the physical fields studied in water electrolyzers, the use of a magnetic field is particularly promising due to magnetohydrodynamic (MHD) and magnetoaerodynamic (MAD) effects on the flow regions. In the liquid phase, MHD (Lorentz force) is more effective while in the gas phase MAD (Kelvin force) is more dominant. Applying an external magnetic field in perpendicular position to the current direction generates Lorentz Force, which ensures the convection of bubbles inside the cell [27]. Under the magnetic field, when current is perpendicular to the magnetic field, buoyancy force and Lorentz force push and separate the bubbles from the electrode surface. This improves mass transfer inside the cell. On the other hand, in the gas phase, due to the related magnetic properties of the gasses they can move in

different directions. It is commonly known that  $H_2$  is diamagnetic gas but  $O_2$  is a paramagnetic gas. Thanks to the different magnetic properties of  $O_2$  and  $H_2$  gases, the magnetic field provides a moving force and orientation. This provides enhanced proton transfer through the membrane and better gas separation from the electrodes resulting in better mass transfer [27, 28].

Several studies in the literature reported an enhanced electrochemical cell performance under external magnetic field [29, 30]. The performance of different types of fuel cells under magnetic field was also investigated [31-33]. Furthermore, the effect of magnetic field on oxygen and hydrogen evolution reactions and the species transport in electrolyzers was studied [27, 28, 34]. Here, the effect of magnetic field in water electrolysis is very promising, especially in terms of the bubble separation from the electrode surface resulting in reduced mass transfer and ohmic losses and enhanced electrolyzer performance. We have recently demonstrated the positive effect of the application of an external magnetic field on the performance of PEMWEs [35].

Moreover, as oxygen is a paramagnetic molecule, the magnetic field can influence its direction [36]. Thus, it is possible to enhance its interaction with the electrode at the micro level by modifying the electrocatalyst through magnetizing the reaction interface or the material. Some studies investigated magnetically modified catalysts for electrochemical applications [37-39]. Li et al.[39] investigated the magnetic field effect on the oxygen evolution reaction in the magnetic  $Co_3O_4$  semiconductor catalyst. They stated that the magnetic field increases the electrons spin energy and charge transfer kinetics in the catalyst. These factors not only improve the charge transport in the OER catalytic reaction substantially but also avoid the need for complex catalyst structural modification, morphological control, and material cladding. Moreover, they reported that the magnetic field provides easily controllable morphology and coatings by the help of its effect on the electrode surface. Okada et al.[37] studied Nd/Fe/B magnetic particles by directly applying it on the cathode catalyst layer of an PEM fuel cell to observe the effect on performance. The catalyst performance was studied ex-situ using a

rotating disk electrode and higher current density and limiting current were obtained with the magnetized catalyst. Recently, Shi et al. [38] studied a magnetically modified catalyst for PEM fuel cells. They used Pt-Nd<sub>2</sub>Fe<sub>14</sub>B catalyst at the cathode and obtained four times increase in performance due to Kelvin force effect. Despite the promising results in PEM fuel cells, to the authors knowledge, there are no studies reported on the effect of applying magnetically modified catalyst in PEMWE.

In this study, the commonly used PEMWE anode catalyst (IrO<sub>2</sub>) was modified with the magnetic Fe<sub>3</sub>O<sub>4</sub> to investigate its effect on PEMWE performance. Thus, 90% IrO<sub>2</sub> - 10% Fe<sub>3</sub>O<sub>4</sub> and 80% IrO<sub>2</sub> - 20% Fe<sub>3</sub>O<sub>4</sub> samples were prepared and tested ex-situ in an electrochemical cell and in-situ in a PEMWE single cell. The results of non-magnetized and magnetized samples were compared to study the effect of the magnetic composite catalyst layer on the cell performance.

## **2. Experimental**

### **2.1. Synthesis of IrO<sub>2</sub>/Fe<sub>3</sub>O<sub>4</sub> composites using Adam's Fusion Reaction**

To prepare the catalyst in oxide structure, a modified Adam's Fusion method was used [40]. In this method, to obtain IrO<sub>2</sub>, IrCl<sub>3</sub>.H<sub>2</sub>O (99.9%, Aldrich) precursor was used. In addition, IrCl<sub>3</sub>.H<sub>2</sub>O (99.9%, Aldrich) was used with FeCl<sub>2</sub> and FeCl<sub>3</sub> to obtain 80% IrO<sub>2</sub> - 20% Fe<sub>3</sub>O<sub>4</sub>, 90% IrO<sub>2</sub> - 10% Fe<sub>3</sub>O<sub>4</sub>, respectively. FeCl<sub>2</sub>.H<sub>2</sub>O (98%, Aldrich) and FeCl<sub>3</sub>. H<sub>2</sub>O (≥99.9%, Aldrich) were used to achieve 1/1.75 ratio of Fe<sup>2+</sup>/Fe<sup>3+</sup> and produce the IrO<sub>2</sub>/ Fe<sub>3</sub>O<sub>4</sub> composites [3, 40-42]. To prepare the composites, the relevant amount of IrCl<sub>3</sub>. H<sub>2</sub>O, FeCl<sub>2</sub>. H<sub>2</sub>O and FeCl<sub>3</sub>. H<sub>2</sub>O were dissolved in distilled water. Then 5 g of finely ground NaNO<sub>3</sub> (99.995%, Aldrich) was added to the solution and a homogeneous mixture was obtained. All mixtures were placed on a magnetic stirrer for about 1 hour to obtain homogeneous solutions.

Then, the mixtures were placed in a preheated oven at 80 °C to evaporate the water. The dried catalysts were placed in ceramic crucibles and sintered at 500 °C in air for one hour. The metal oxides obtained were then cleaned with distilled water and centrifuged. Finally, the metal oxide catalyst powders were dried in a vacuum oven at 80 °C. The prepared catalyst powders were then characterised with Scanning Electron Microscope (SEM) and Energy Dispersive X-Ray Analysis (SEM –EDX) under a 15kV electron beam using a table top SEM (Hitachi TM3030 plus) and X-Ray Powder Diffraction (XRD) (Bruker D2 benchtop, Co Tube) and X-ray Photoelectron Spectroscopy (XPS)(SPECS Inc.). Finally, Brunauer-Emmett-Teller (BET) measurement was conducted to obtain adsorption and desorption isotherms and find the catalyst surface area and average pore diameter. The test was conducted using a Micromeritics 3Flex BET surface area and microporosity measurement device.

Two composite catalyst compositions were investigated in this study, namely; 90% IrO<sub>2</sub> - 10% Fe<sub>3</sub>O<sub>4</sub> and 80%IrO<sub>2</sub> - 20%Fe<sub>3</sub>O<sub>4</sub>. The composites were prepared by mixing catalyst inks with the relevant metal loading to obtain the targeted loading ratios. The indicated percent value in the composite name indicates molar percent in the compound.

## **2.2. Samples Preparation for Electrochemical Cell Testing**

The electrochemical tests were conducted both in an electrochemical three-electrode wet cell, and in-situ in a single polymer electrolyser cell. For the electrochemical wet cell, the catalyst powders were mixed in with the 5% Nafion® perfluorinated resin solution (5 wt. % in lower aliphatic alcohols and water, contains 15-20% water Aldrich) and ultrapure distilled water (Milli-Q®). The mixture was dispersed with an ultrasonic probe at 0.5 amplitude with 30 pulses for about 15 minutes to obtain a catalyst ink. A glassy carbon (GC) working electrodes (7.065 mm<sup>2</sup> surface area) were prepared with a total of 2.8 mg metals loading at different molar ratios. The catalyst was deposited on the clean GC electrodes via a micropipette, and then their

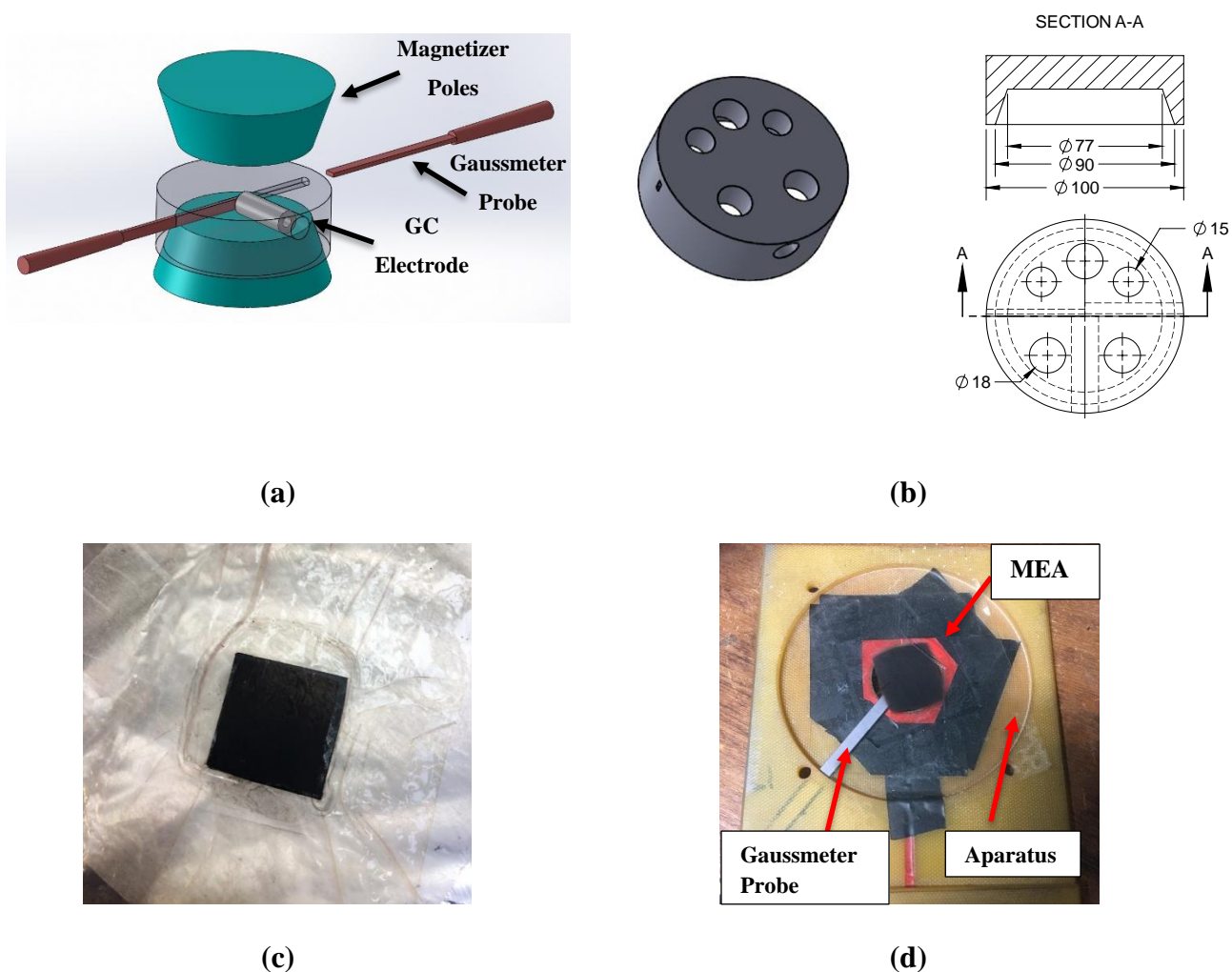


magnetized and non-magnetized performance was investigated. A three-electrode configuration was used in an electrochemical cell, with 0.5 M H<sub>2</sub>SO<sub>4</sub> as the electrolyte solution. The reference, counter and working electrodes were a saturated Ag/AgCl (206 mV potential shift compared to SHE), bright Pt mesh, and the GC electrode with the deposited catalyst respectively. A computer-controlled AMETEK ® Verstatat 3 Potentiostat was used to record linear-sweep voltammetry (LSV) and Chronoamperometry Analysis (CA). The LSV was obtained within the potential range of (0.0 -1.7 V vs. Ag/AgCl) at scan rate of 50mV s<sup>-1</sup> and CA analysis are conducted for 40000 s at 1.5 V.

Moreover, PEMWE cell tests were conducted to observe the performance of the magnetized and non magnetized catalysts *in-situ* in a single cell PEMWE. Thus, a Membrane Electrode Assembly (MEA) with 5 cm<sup>2</sup> active area was used to validate the LSV results. Here, a Nafion 115 membrane was coated with 3 mg cm<sup>-2</sup> anode catalyst using an airbrush and vacuum table to prepare catalyst coated membranes (CCM). Then, 0.4 mg cm<sup>-2</sup> of Pt (20% Platinum on Vulcan XC 72-E-TEK) catalyst were coated on a Toray TGP-H-120-PTFE gas diffusion layer (GDL), respectively to obtain the cathode electrode. All components were assembled in an MEA by hot-pressing at 140 °C for 2 minutes. The MEA was then placed in a PEMWE single cell holder with a Pt coated Ti mesh as the anode GDL, and between two Ti current collectors. A gear pump was used to supply water to the PEMWE and the flow rate was fixed at 100 ml min<sup>-1</sup> for all experiments. Polarization curves (V-I) are obtained by an IviumStat XRI potentiostat in LSV mode with 10 mV s<sup>-1</sup> scan rate between 0.0-2.5 V. Firstly, the non-magnetized samples were tested at 40 °C and 80 °C and then the samples were magnetized and tested at the same conditions.

## 2.3. Magnetization Method of the Samples

The modified GC electrodes and MEAs were magnetized by placing them in a specially designed holder within a magnetizer (Newport Instruments-Farnell). The magnetizer has an adjustable field strength and up to 2 T magnetic flux was used to modify the GC electrodes and MEAs (see Figure 1). The GC holder was made in-house, 3-D printed from PLA (non-conductive), with ports for the GC electrode and gaussmeter probe. All equipments for magnetization are designed for the saturation of the particles in relevant amount of magnetization.



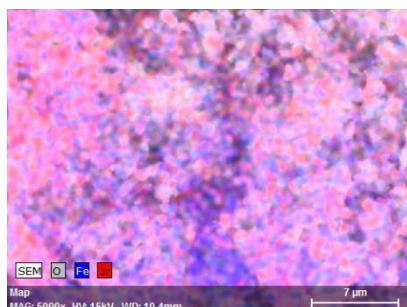
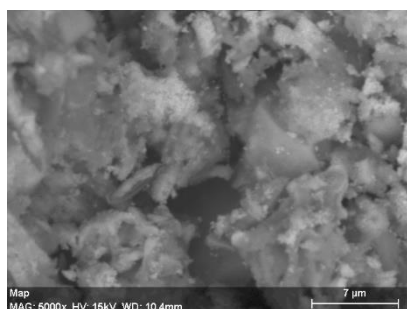
**Figure 1.** a) Magnetization apparatus design for the GC electrodes, b) 3D printed design , c) prepared MEA for magnetization and d) magnetization apparatus for MEAs.

To measure the particles magnetization level, horizontal and vertical gauss meter probe holes were introduced. In Figure 1.b, the top view and the cross-section of the equipment can be seen. Figure 1.c and 1.d present the MEA and its position on magnetization apparatus. The main advantage of the MEA magnetization apparatus is minimising the distance between the N-S poles. The generated magnetic flux density was measured using a LakeShore 455 DSP gaussmeter which has 10  $\mu$ T sensitivity. The prepared MEAs were assembled and tested with the magnetized and non-magnetized conditions, respectively.

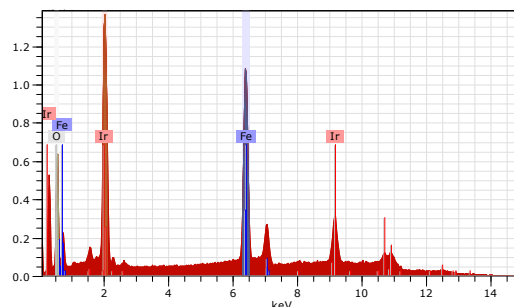
### **3. Results and Analysis**

#### **3. 1. Catalyst Materials Characterization**

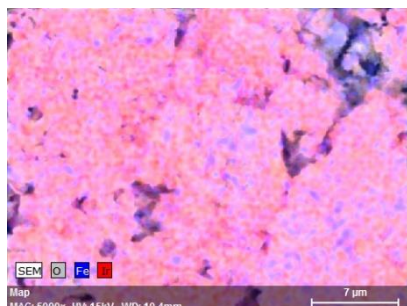
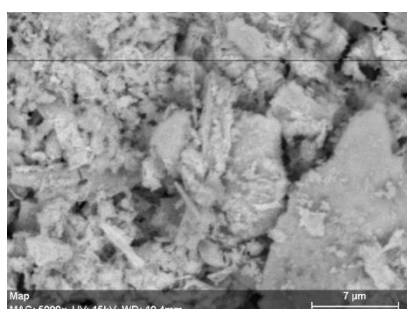
Firstly, the prepared metal oxide catalysts were physically characterised via SEM-EDX, XRD, and BET surface area to determine their composition and structure before conducting the electrochemical tests. Fig. 2 shows the SEM-EDX images for 80%  $\text{IrO}_2$  - 20%  $\text{Fe}_3\text{O}_4$  and 90%  $\text{IrO}_2$ -10%  $\text{Fe}_3\text{O}_4$  composite structures.



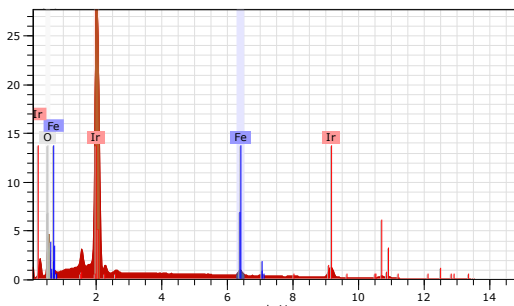
Element	wt. %	Atomic Percent
Iridium	54.07	14.55
Iron	27.33	25.32
Oxygen	18.60	60.13
Totals	100	100



(a)



Element	wt. %	Atomic Percent
Iridium	68.61	16.31
Iron	2.94	2.40
Oxygen	28.45	81.28
Totals	100	100

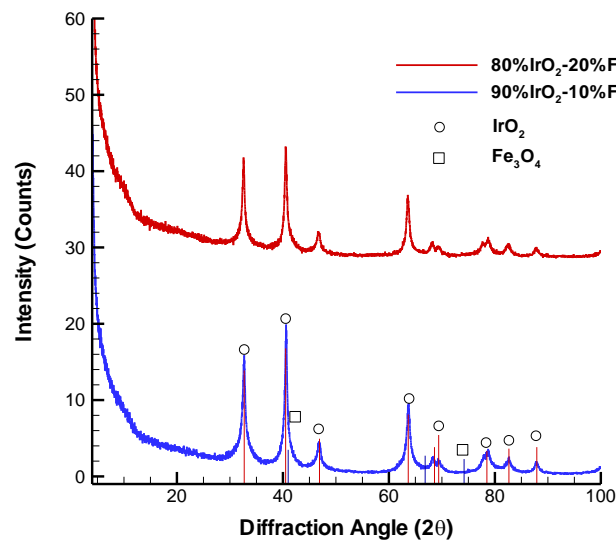


(b)

**Figure 2.** SEM EDX images for a) 80% IrO<sub>2</sub> - 20% Fe<sub>3</sub>O<sub>4</sub> and b) 90% IrO<sub>2</sub> -10% Fe<sub>3</sub>O<sub>4</sub> samples

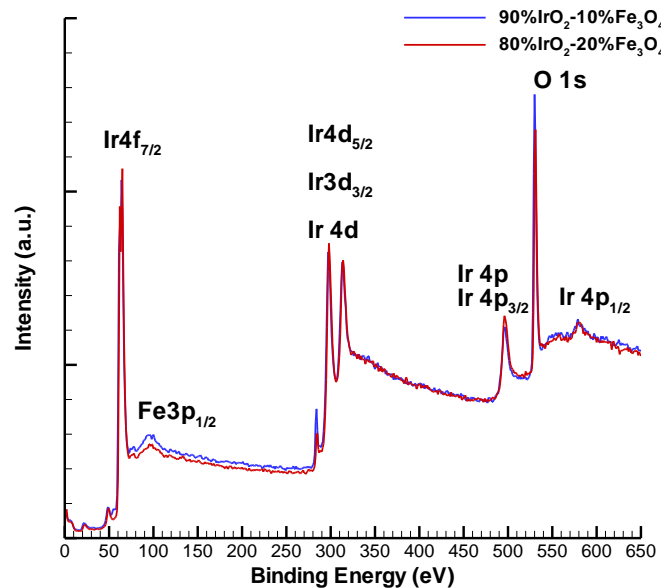
The SEM and EDX images indicate that Ir, Fe and O are present in both samples and appear to be distributed homogeneously in the catalyst, and the presence of both Fe and Ir metal-oxides in the catalyst samples. Moreover, the EDX confirms that the amount of Fe is lower in 90%

IrO<sub>2</sub>-10% Fe<sub>3</sub>O<sub>4</sub> than in 80% IrO<sub>2</sub>-20 %Fe<sub>3</sub>O<sub>4</sub>, as expected. Next, the XRD patterns were recorded for the two composites and can be seen in Figure 3.



**Figure 3.** XRD patterns for 80%IrO<sub>2</sub>-20%Fe<sub>3</sub>O<sub>4</sub> and b) 90%IrO<sub>2</sub>-10%Fe<sub>3</sub>O<sub>4</sub> samples

The IrO<sub>2</sub> peaks in the XRD patterns can be seen clearly and fit with literature data [43]. The Fe<sub>3</sub>O<sub>4</sub> peak regions [44] are very close to that for IrO<sub>2</sub> and due to the low amount in both samples the peaks cannot be observed clearly in the XRD pattern. However, there are slight shift in the peaks due to the different Fe<sub>3</sub>O<sub>4</sub> and IrO<sub>2</sub> molar ratios. Therefore, XPS analysis was conducted to validate Fe<sub>3</sub>O<sub>4</sub> structures as shown in Figure 4.



**Figure 4.** XPS analysis for different composite samples

As seen in Fig.4, Fe peak on  $3p_{1/2}$  indicating the presence of  $\text{Fe}_3\text{O}_4$  can be observed at 53.9 eV binding energy [57, 58]. Moreover, on the 60.7, 300, 520 and 550 eV values, Ir peaks can be seen further confirming the presence of  $\text{IrO}_2$  [59].

Finally, Table 1 provides a comparison of the BET results of the composite catalysts prepared in this work against the synthesised  $\text{IrO}_2$ . As can be seen in Table 1, BET surface area is highest in synthesized  $\text{IrO}_2$  catalysts with  $135.53 \text{ m}^2 \text{ g}^{-1}$  value, and is reduced with the introduction of  $\text{Fe}_3\text{O}_4$ . The 90%  $\text{IrO}_2$ -10%  $\text{Fe}_3\text{O}_4$  sample, has a surface area and pore diameter values very close to that measured for  $\text{IrO}_2$ , however, significant reduction in surface area and increase in porosity is shown for 80%  $\text{IrO}_2$ -20%  $\text{Fe}_3\text{O}_4$  due to the reduced  $\text{IrO}_2$  loading and increased  $\text{Fe}_3\text{O}_4$  loading.

**Table 1.** BET surface area analysis of different samples and average pore diameters.

	BET Surface Area / $\text{m}^2 \text{ g}^{-1}$	Average pore diameter / nm
Synthesized $\text{IrO}_2$	135.53	4.40
90% $\text{IrO}_2$ -10% $\text{Fe}_3\text{O}_4$	131.3	4.6
80% $\text{IrO}_2$ -20% $\text{Fe}_3\text{O}_4$	108.9	8.6

### 3.2. Magnetization of Electrode Materials

The GC and MEA samples were magnetized, and their magnetization level were measured, respectively. Table 2 shows the applied and measured magnetic flux density for the samples examined in the study.

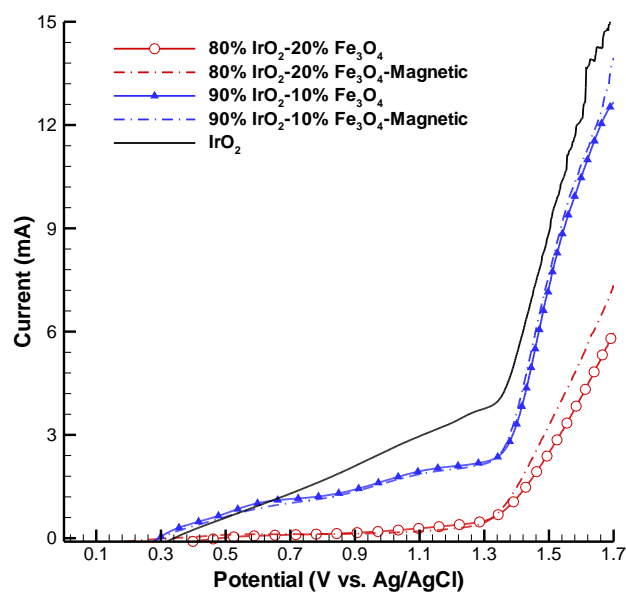
**Table 2.** Applied and measured magnetic flux amount on the samples

Sample	Applied Magnetic Flux Amount with Magnetizer / T	Magnetization Time / min	Measured Magnetic Flux Amount on The Sample Surface / mT	Measured Magnetic Flux Difference on The Sample After Magnetization / mT
80% IrO <sub>2</sub> - 20% Fe <sub>3</sub> O <sub>4</sub> on GC	1.6	3	0.192	0.072
90% IrO <sub>2</sub> - 10% Fe <sub>3</sub> O <sub>4</sub> on GC	1.6	3	0.182	0.036
80% IrO <sub>2</sub> - 20% Fe <sub>3</sub> O <sub>4</sub> on MEA	2	3	1.92	0.31
90% IrO <sub>2</sub> - 10% Fe <sub>3</sub> O <sub>4</sub> on MEA	2	3	1.93	0.22

As seen in Table 2, The degree of magnetization is quite low with 0.072 and 0.036 mT for GC electrodes with the 80% IrO<sub>2</sub> - 20% Fe<sub>3</sub>O<sub>4</sub> and 90% IrO<sub>2</sub> - 10% Fe<sub>3</sub>O<sub>4</sub> catalysts, respectively. This is due to the low surface area of the GC (9.62 mm<sup>2</sup>). Thus, a 5 cm<sup>2</sup> surface area of MEA was coated with the composite catalysts and magnetized to observe the effect of magnetic particles on a larger surface. After magnetization, the measured magnetic flux difference in the MEA samples were 0.31 and 0.22 mT for 80% IrO<sub>2</sub> - 20% Fe<sub>3</sub>O<sub>4</sub> and 90% IrO<sub>2</sub> - 10% Fe<sub>3</sub>O<sub>4</sub>, respectively.

### 3.3. Analysis of electrochemical performances

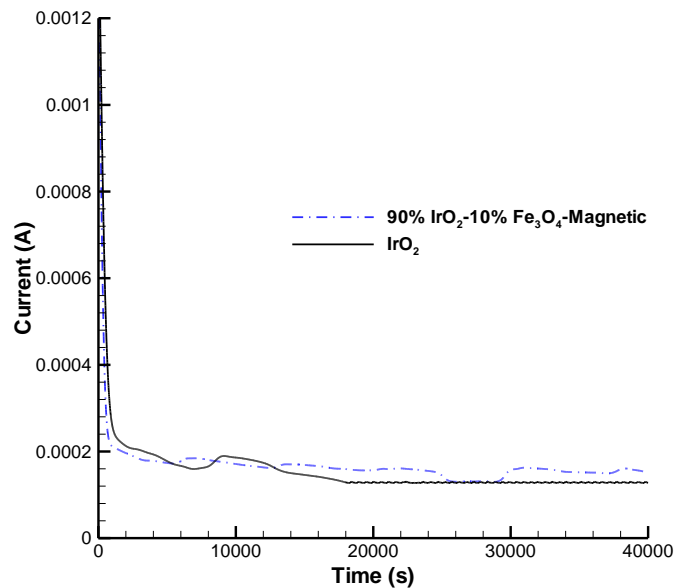
To measure the electrochemical performance of the magnetized samples, LSV experiments were conducted. Firstly, LSV measurements of magnetized and non-magnetized particles were measured as shown in Figure 5.



**Figure 5.** LSV curves for samples

With the addition of Fe<sub>3</sub>O<sub>4</sub> to the IrO<sub>2</sub> for both samples (20% and 10% respectively), the performance of the catalyst decreases due to the lower catalytic activity of Fe<sub>3</sub>O<sub>4</sub> and the reduction of IrO<sub>2</sub> loading. However, when these samples are magnetized at 1.6 T, the LSV curves are shifted closer towards the IrO<sub>2</sub> performance. The change in the LSV is mainly noticed at higher current density and therefore in the mass transport region. The improvement of current achieved at constant voltage for the 80%IrO<sub>2</sub>-20%Fe<sub>3</sub>O<sub>4</sub> sample after magnetisation is around 22% at 1.7 V.

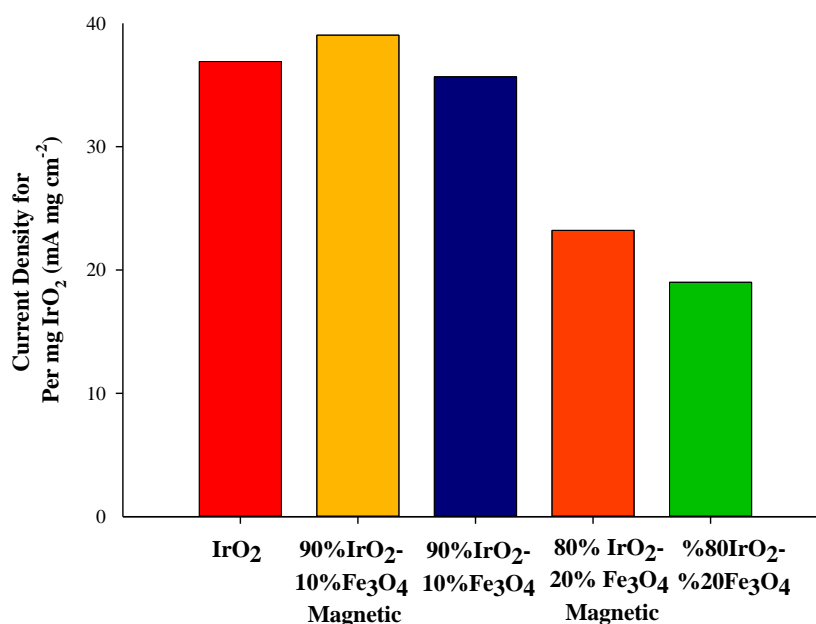




**Figure 6.** CA measurements for %90 IrO<sub>2</sub>-%10 Fe<sub>3</sub>O<sub>4</sub> and IrO<sub>2</sub>

As seen in Figure 6, the CA measurements show the stability of Fe<sub>3</sub>O<sub>4</sub> containing catalyst compared to pristine IrO<sub>2</sub> at 1.5 V. The detected increase in magnetic flux from the sample after magnetization is shown in Table 2, further confirming the presence and stability of magnetic effect in the catalyst layer in the MEA.

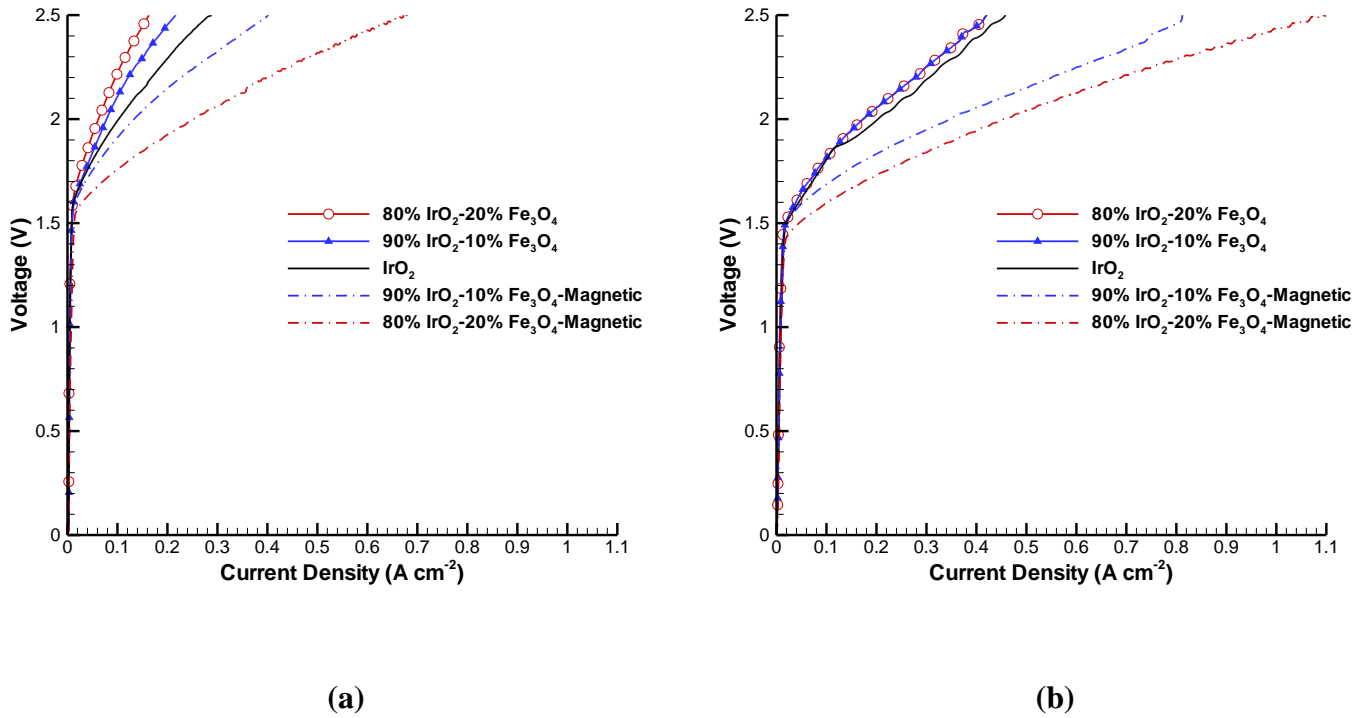
Figure 7 shows the maximum current density value obtained for each sample per mg of IrO<sub>2</sub>. It is clear that the magnetized samples have a better performance at 1.7 V vs Ag/AgCl. Here, with 10 % Fe<sub>3</sub>O<sub>4</sub> loading, the performance improvement from magnetisation is 9.5 %, and with 20 % Fe<sub>3</sub>O<sub>4</sub> loading the performance improvement is around 22.2 %. Moreover, the 90% IrO<sub>2</sub>-10% Fe<sub>3</sub>O<sub>4</sub> showed relatively higher performance than that achieved by the pristine IrO<sub>2</sub> catalyst.



**Figure 7.** Current density value for per mg IrO<sub>2</sub> from the ex-situ LSV analysis

It can be concluded from these results that by magnetising the catalyst layer, higher current density can be achieved than that from a pristine IrO<sub>2</sub> catalyst layer. If such catalyst is used in a stack, they would decrease the amount of IrO<sub>2</sub> usage and as a result reduce the stack cost. These results are in line with expectations from the earlier review of the literature [38, 45]. Moreover, Tufa et al. [46] recently published the use of magnetic Ag@Fe<sub>3</sub>O<sub>4</sub> magnetoplasmonic electrodes to observe the effect of Kelvin and Lorentz Force on electrochemical performance. They concluded that the magnetic flux applied on the electrode magnetized the Ag@Fe<sub>3</sub>O<sub>4</sub> film. As a result, a highly nonuniform magnetic field, inducing Kelvin force near to the working electrode, is generated at the film surface. In their EIS analysis, the magnetic MagPlas3 film had bigger electron transfer and conductivity values. Moreover, when the samples were magnetized, the achieved current value increased from  $3.5 \times 10^{-5}$  A to  $4 \times 10^{-5}$  A. Thus, their reported results are in good agreement with the result achieved in this study.

Next, MEA testing was carried out to investigate if these promising ex-situ results could be replicated in a single-cell PEMWE. Figure 8 shows the results from the experiments carried out at 40 and 80 °C.

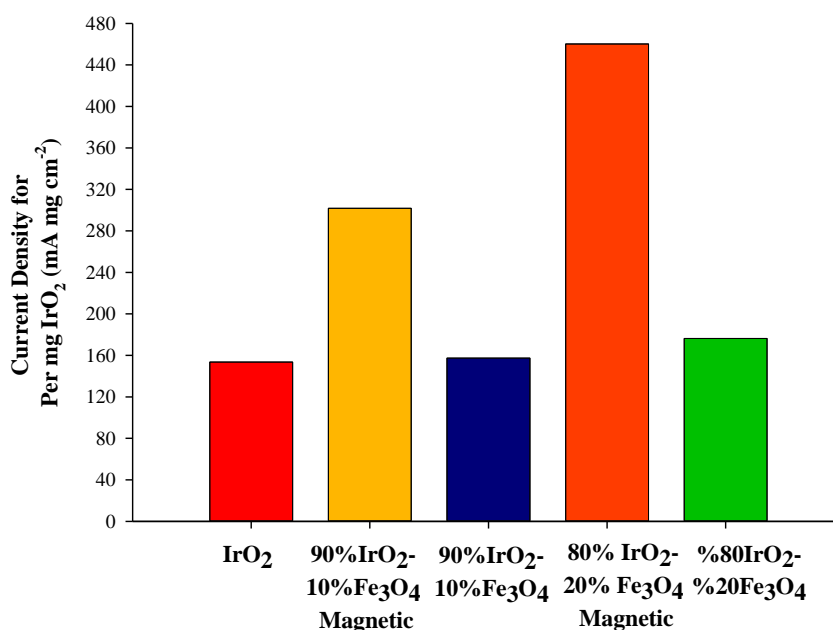


**Figure 8.** PEMWE Cell tests for composite samples a) at 40 °C, b) at 80 °C

According to Fig.8.a, IrO<sub>2</sub> had a better performance than the MEAs with catalyst containing non-magnetic 10% Fe<sub>3</sub>O<sub>4</sub> and 20% Fe<sub>3</sub>O<sub>4</sub> loading. By increasing the amount of Fe<sub>3</sub>O<sub>4</sub> by 20%, the catalyst performance is decreased by around 20%. On the other hand, when the catalyst in the MEAs is magnetized in the magnetizer at 2 T, the samples containing 10% and 20% Fe<sub>3</sub>O<sub>4</sub> display better performance than the pristine IrO<sub>2</sub>. Particularly for the sample with 20% Fe<sub>3</sub>O<sub>4</sub> loading where four times of the maximum current density for IrO<sub>2</sub> was achieved. With the 10% Fe<sub>3</sub>O<sub>4</sub> sample, the improvement of performance is around 2.5 times higher than the non-magnetized sample. These results echo the behaviour seen in LSV measurements.

Moreover, as the conductivity and magnetic properties of Fe<sub>3</sub>O<sub>4</sub> are reduced at higher temperature [47], the improvement in the electrolyser cell performance is more significant at

40 °C. The performance, as seen in Figure 9, shows the improvement in the performance in the mass transfer region and ohmic region of the polarization curve. Figure 8.b presents similar behaviour to that seen at 40 °C, however the performance for the catalyst layer with 10 % and 20 %  $\text{Fe}_3\text{O}_4$  loading is very close. At higher temperatures the activation polarization losses in the cell are lowered for all samples. When the samples with 10% and 20%  $\text{Fe}_3\text{O}_4$  are magnetized, the current density value is increased significantly. The increase in the current density of the 20%  $\text{Fe}_3\text{O}_4$  loading catalyst is twice of that of the non-magnetized sample. On the other hand, at 10%  $\text{Fe}_3\text{O}_4$  loading, 1.5 times increase in the current density is achieved with magnetisation. In Figure 9, at 80°C, the maximum current density value obtained for each sample for per mg of  $\text{IrO}_2$  can be seen.



**Figure 9.** Current density value for per mg  $\text{IrO}_2$  from polarization curve at 80 °C

As seen in Figure 9, The addition of  $\text{Fe}_3\text{O}_4$  before magnetization did not affect the maximum current density value per mg  $\text{IrO}_2$ . However, after magnetization, the 80%  $\text{IrO}_2$  - 20%  $\text{Fe}_3\text{O}_4$  and 90%  $\text{IrO}_2$  - 10%  $\text{Fe}_3\text{O}_4$  composite catalysts the maximum current density per mg  $\text{IrO}_2$  is substantially increased. Moreover, the higher the magnetic  $\text{Fe}_3\text{O}_4$  loading, the higher the

increase in current density. The catalyst layer with 80% IrO<sub>2</sub> - 20% Fe<sub>3</sub>O<sub>4</sub> sample, the maximum current density per mg IrO<sub>2</sub> increased from 176.2 mA cm<sup>-2</sup> to 460.2 mA cm<sup>-2</sup> and for 90% IrO<sub>2</sub> - 10% Fe<sub>3</sub>O<sub>4</sub> sample, the maximum current density per mg IrO<sub>2</sub> increased from 157.3 mA cm<sup>-2</sup> to 301.8 mA cm<sup>-2</sup>. It is possible to explain these effects on the gas phase phenomenon of magnetic forces. In liquid phase, the Lorentz force is dominant, but in the gas phase the Kelvin force affects the gas particles. O<sub>2</sub> which is paramagnetic gas, changes its direction through the magnetic flux direction. Thus, at the anode side, the ferromagnetic Fe<sub>3</sub>O<sub>4</sub> particles enhance O<sub>2</sub> bubbles removal, accelerates their flow away from the catalyst active sites, and therefore increase the performance of the PEMWE.

#### 4. Conclusion

Using Adam's fusion reaction, IrO<sub>2</sub> catalyst was synthesized successfully. Moreover, composite catalyst of IrO<sub>2</sub>-Fe<sub>3</sub>O<sub>4</sub> with different molar ratios was synthesized for the first time in the literature by a Modified Adam's Fusion Method. The synthesized catalysts were then coated on a GC and made into an MEA to study their *ex-situ* and *in-situ* electrochemical performance, respectively, and observe the catalyst magnetization effect. The results demonstrate, both in *ex-situ* and *in-situ*, an improvement in the composite catalyst electrochemical performance with magnetization. The magnetized catalyst layer achieved around 2.5- and 4-fold increase in the MEA maximum current density, at 10% and 20% Fe<sub>3</sub>O<sub>4</sub> respectively, in comparison to the non-magnetized and pristine IrO<sub>2</sub> catalyst. This improvement was observed at both operating temperatures examined, namely, 40 °C and 80 °C.

It is important to highlight here that despite the decrease in the IrO<sub>2</sub> loading in the composite catalyst layer, significantly higher performance was achieved. In this study, the highest performing catalyst layer (80% IrO<sub>2</sub> - 20% Fe<sub>3</sub>O<sub>4</sub>) had 20% less IrO<sub>2</sub> which was replaced by the abundant and cheap Fe<sub>3</sub>O<sub>4</sub> (1 gr of IrO<sub>2</sub> is 300\$ compared to 20\$ for 1 gram). Therefore, a significant decrease in the cost of the catalyst layer and therefore the electrolyzer can be realized

by employing the magnetic composite catalysts developed in this study. In the future, other magnetic oxides like  $\text{CrO}_2$ ,  $\text{Fe}_2\text{O}_3$  will be studied to investigate their magnetization effect and corrosion performance as anode catalyst for PEMWE studies.

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